

GEOTECHNICAL INVESTIGATION AND ACID SULFATE SOIL ASSESSMENT

FOR

NSW Land & Housing Corporation

18 – 28 Simpson Street, Dundas Valley, New South Wales (BGYJW)

Report No: 21/3669

Project No: 31527/5761D-G

December 2021



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DRAWING NO. 21/3669 – BOREHOLE AND PENETROMETER LOCATIONS
NOTES RELATING TO GEOTECHNICAL REPORTS

APPENDIX A - BOREHOLE LOGS AND EXPLANATION SHEETS

APPENDIX B - LABORATORY TEST RESULTS



1. INTRODUCTION

This report presents the results of a combined Geotechnical Investigation and Acid Sulfate Soil (ASS) assessment carried out by STS Geotechnics Pty Limited (STS) for a proposed new residential development to be constructed at 18 – 28 Simpson Street, Dundas Valley, New South Wales ("the site"). At the time of writing this report STS were not provided with architectural drawings for the project, however we understand the development will typically comprise the construction of single and double storey residential buildings. The development will not include basement levels. Reference to the Parramatta LEP indicates the site is located within a Class 5 Acid Sulfate Soils area and therefore Council requires an assessment to be undertaken.

The purpose of the investigation was to:

- assess the subsurface conditions over the site,
- provide a Site Classification to AS2870,
- provide recommendations regarding the appropriate foundation system for the site including design parameters,
- · comment on soil aggressiveness to buried steel and concrete,
- undertake an ASS assessment, and
- determine if an ASS Management Plan is required.

The investigation was undertaken at the request of NSW Land and Housing Corporation.

Our scope of work did not include a contamination assessment.

2. NATURE OF THE INVESTIGATION

2.1. Fieldwork

The fieldwork consisted of drilling eight (5) boreholes numbered BH1 to BH8, inclusive, at the locations shown on Drawing No. 21/3668. Restricted site access dictated the borehole locations. The boreholes were drilled using a track mounted Christie drilling rig owned and operated by STS. Soils and weathered rock were drilled using rotary solid flight augers. Soil strengths were determined by undertaking Dynamic Cone Penetrometer (DCP) tests at each borehole location. Drilling operations were undertaken by one of STS's technical officers who also logged the subsurface conditions encountered.

The subsurface conditions observed are recorded on the borehole logs given in Appendix A. An explanation of the terms used on the logs is also given in Appendix A. Notes relating to geotechnical reports are also attached.

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2.2. Laboratory Testing

To assist with determining the site classification, shrink swell index tests were carried out on representative samples retrieved from the site.

To assess the soils for their aggressiveness, selected representative soil samples were tested to determine the following:

- pH,
- Sulphate content (SO₄),
- Chloride content (CL), and
- Electrical Conductivity (EC)

Detailed test reports are given in Appendix B.

3. GEOLOGY AND SITE CONDITIONS

The Sydney geological series sheet at a scale of 1:100,000 shows Triassic Age Ashfield Shale of the Wianamatta Group underlies the site. Rocks within this formation comprise mainly shale and laminite.

The site is roughly rectangular in shape with an area of approximately 2590 m². At the time of the fieldwork, brick residential buildings were present on the site. Site vegetation comprised grass, trees and shrubs.

The ground surface falls approximately 2 metres to the east. Single and double storey residential dwellings are present in the nearby properties.

4. SUBSURFACE CONDITIONS

When assessing the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour regarding the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies, particularly on sites such as this where there has been previous development.

The subsurface conditions generally consist of topsoil and fill overlying silty clays and weathered shale. Fill was encountered in BH4 to a depth of 0.6 metres. In the remaining boreholes topsoil was encountered to approximate depths of 0.2 to 0.6 metres. Firm to stiff becoming very stiff natural silty clays underlie the fill and topsoil to depths of 0.85 to 1.5 metres. Weathered shale underlies the natural soils to the auger refusal depths of 1.3 to 1.9 metres.

Groundwater was not observed during drilling of the boreholes.



5. GEOTECHNICAL DISCUSSION

5.1. Site Classification to AS2870

The classification has been prepared in accordance with the guidelines set out in the "Residential Slabs and Footings" Code, AS2870 – 2011.

Undisturbed samples were obtained to determine their shrink swell index. The results are summarised in Table 5.1

Table 5.1 – Shrink Swell Summary

Location	Depth (m)	Material Description	Shrink/Swell Index (% per ∆pF)		
BH1	0.7-0.9	Red brown gravelly sandy clay	1.8		
BH3	0.7-0.85	Orange brown gravelly sandy clay	0.8		
BH5	0.7-0.9	Red brown silty clay	2.9		
ВН7	0.7 – 0.9	Red brown and yellow gravelly silty clay	1.6		

Because of the trees and dwellings present, abnormal moisture conditions (AMC) prevail at the site. (Refer to Section 1.3.3 of AS2870).

Because of the AMC present, the site is classified *a problem site* (*P*). However, provided the recommendations given below are adopted and the footings bear in the underlying natural soils, the site may be reclassified *highly reactive* (*H*1).

5.2. Foundation Design

The existing topsoil and fill materials should not be relied upon for foundation support. Footings that bear in the stiff natural clayey soils may be proportioned using an allowable bearing pressure of 100 kPa. The minimum depth of founding must comply with the requirements of AS2870-2011. To overcome the presence of the trees along the site boundaries, the foundations should be designed in accordance with the procedures given in Appendices H and CH of AS2870-2011. Tree information is attached.

Should a higher bearing pressure be required then piles can be used. Piles founded in weathered shale may be proportioned using an allowable bearing pressure of 700 kPa. An allowable adhesion of 70 kPa may be adopted for the portion of the shaft within the weathered shale. When piles are founded in shale the adhesion within the overlying soils must be ignored.

To ensure the bearing values given can be achieved, care should be taken to ensure that the base of excavations is free of all loose material prior to concreting. It is recommended that all footing excavations be protected with a layer of blinding concrete as soon as possible, preferably immediately after excavating, cleaning, inspection and approval. The possible presence of groundwater needs to be considered when drilling piers and pouring concrete.



5.3. Soil Aggressiveness

The aggressiveness or erosion potential of an environment in building materials, particularly concrete and steel is dependent on the levels of soil pH and the types of salts present, generally sulphates and chlorides. To determine the degree of aggressiveness, the test values obtained are compared to Tables 6.4.2 (C) and 6.5.2 (C) in AS2159 – 2009 Piling – Design and Installation. The test results are summarised in Table 5.2 below.

Table 5.2- Soil Aggressiveness Summary Table

Sample No.	Location	Depth (m)	рН	Sulfate (mg/kg)	Chloride (mg/kg)	Condu	trical activity /m)
						EC _{1:5}	ECe
S1	BH1	0.4	5.9	<10	120	0.030	0.3
S2	BH2	0.4	5.4	<10	40	0.014	0.1
S3	BH4	0.4	5.9	10	60	0.019	0.2
S4	BH5	0.4	5.1	30	<10	0.034	0.3
S5	вн6	0.4	6.3	10	90	0.019	0.2
S6	BH8	0.4	5.6	40	20	0.036	0.3

The soils on the site are cohesive in nature. Therefore, the soil conditions B are considered appropriate.

A review of the durability aspects indicates that:

• pH : minimum value of 5.1

SO₄: maximum value of 40 mg/kg (ppm) > 5000 ppm
Cl: maximum value of 120 mg/kg (ppm) < 5000 ppm

• EC_e : maximum value of 0.3 dS/m

In accordance with AS2159-2009, the exposure classification for the onsite soils is non-aggressive to steel and mildly aggressive to concrete. In accordance with AS2870-2011 the soils are classified as A2.

Reference to DLWC (2002) "Site Investigations for Urban Salinity" indicates that the EC $_{\rm e}$ values of 0.1 to 0.3 dS/m are consistent with the presence of non-saline soils.

6. ACID SULFATE SOIL ASSESSMENT

6.1. Introduction

ASS is the common name given to sediments and soils containing iron sulfides which, when exposed to oxygen generate sulfuric acid. Natural processes formed most acid sulfate sediments when certain conditions existed in the Holocene geological period (the last 10,000 years).

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Report No: 21/3669



Formation conditions require the presence of iron-rich sediments, sulfate (usually from seawater), removal of reaction products such as bicarbonate, the presence of sulfate reducing bacteria and a plentiful supply of organic matter. It should be noted that these conditions exist in mangroves, salt marsh vegetation or tidal areas, and at the bottom of coastal rivers and lakes.

The relatively specific conditions under which acid sulfate soils are formed usually limit their occurrence to low lying parts of coastal floodplains, rivers and creeks. This includes areas with saline or brackish water such as deltas, coastal flats, backswamps and seasonal or permanent freshwater swamps that were formerly brackish. Due to flooding and stormwater erosion, these sulfidic sediments may continue to be re-distributed through the sands and sediments of the estuarine floodplain region. Sulfidic sediment may be found at any depth in suitable coastal sediments – usually beneath the water table.

Any lowering in the water table that covers and protects potential ASS will result in their aeration and the exposure of iron sulfide sediments to oxygen. The lowering in the water table can occur naturally due to seasonal fluctuations and drought or any human intervention, when carrying out any excavations during site development. Potential ASS can also be the exposed to air during physical disturbance with the material at the disturbance face, as well as the extracted material, both potentially being oxidised. The oxidation of iron sulfide sediments in potential ASS results in ASS soils.

Successful management of areas with ASS is possible but must take into account the specific nature of the site and the environmental consequences of development. While it is preferable that sites exhibiting acid sulfate characteristics not be disturbed, management techniques have been devised to minimise and manage impacts in certain circumstances.

When works involving the disturbance of soil or the change of groundwater levels are proposed in coastal areas, a preliminary assessment should be undertaken to determine whether acid sulfate soils are present and if the proposed works are likely to disturb these soils.

6.2. Presence of ASS

Reference to the Prospect-Parramatta ASS Risk Map indicates the property is within an area where there are no known occurrences of Acid Sulfate Soils. It should be noted that maps are a guide only.

The following geomorphic or site criteria are normally used to determine if acid sulfate soils are likely to be present:

- sediments of recent geological age (Holocene)
- soil horizons less than 5 in AHD
- marine or estuarine sediments and tidal lakes
- in coastal wetlands or back swamp areas



6.3. Assessment

The property is at an elevation of between RL 40 and 50 m AHD and is underlain by Ashfield Shale. This is not consistent with the geomorphic criteria necessary for the presence of ASS. Based on our onsite observations and the subsurface conditions exposed in the boreholes, it is our opinion that the proposed construction will not intercept any ASS. As noted above, no groundwater was observed in the boreholes. Therefore, construction will not result in the lowering of any groundwater that may be present in the area.

Our assessment is the proposed construction will not require the preparation of an Acid Sulfate Soil Management Plan.

7. FINAL COMMENTS

During construction, should the subsurface conditions vary from those inferred above, we would be contacted to determine if any changes should be made to our recommendations.

The exposed bearing surfaces for footings should be inspected by a geotechnical engineer to ensure the allowable pressure given has been achieved.

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Laurie Ihnativ

Senior Geotechnical Engineer

STS Geotechnics Pty Limited





Scale: Unknown

Date: December 2021

Client: NSW LAND & HOUSING CORPORATION

GEOTECHNICAL INVESTIGATION
18-28 SIMPSON STREET, DUNDAS VALLEY
BOREHOLE AND PENETROMETER LOCATIONS

Project No. 31527/5761D-G

Drawing No: 21/3669

NOTES RELATING TO GEOTECHNICAL REPORTS

Introduction

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report.

When copies of reports are made, they should be reproduced in full.

Geotechnical Reports

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by STS Geotechnics Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions.
 The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, STS Geotechnics Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

Unforeseen Conditions

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, STS Geotechnics Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows reinterpretation and assessment of the implications for future work.

Subsurface Information

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

Supply of Geotechnical Information or Tendering Purposes

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.



APPENDIX A – BOREHOLE LOGS AND EXPLANATION SHEETS

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpo			В	OREHOLE NO.:	BH 1
1		on Street, Dunc ving No. 21/36				Sheet 1 of 1	
W ATTA EB RL E	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	, P 1	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			TOPSOIL: SILTY CLAY: brown, low plasticity		CL	FIRM TO STIFF	M
	S1 @ 0.4 m	0.5	SILTY CLAY: red brown and mottled orange brown, medium plasticity, trace of gravel	C	CL.	FIRM TO STIFF VERRY STIFF	D-M
	U50						
		1.0					
		1.5	WEATHERED SHALE: grey/brown			EXTREMELY LOW STRENGTH	D
			AUGER REFUSAL AT 1.7 M ON WEATHERED SHALE				
		2.0					
		2.5					
	D - disturbed WT - level of S - jar sampl	f water table o	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT)		nent	: STS : Mini Christie eter (mm): 100	
NOTES:			See explanation sheets for meaning of all descriptive terms and symbols	Angle f Drill Bi		Vertical (°): 0 piral	

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpo		'S No. 31527/5761D-G ember 29, 2021	В	OREHOLE NO.:	BH 2
		wing No. 21/366				Sheet 1 of 1	
W ATTA EBRL E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PROD (Soil type, colour, grain size, plasticity, minor com TOPSOIL: SILTY CLAY: brown, low plasticity		S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			· · · · · · · · · · · · · · · · · · ·				
	S2 @ 0.4 m	0.5	SILTY CLAY: red brown and mottled orange brown, medium plasti	city, trace of gravel	CL	STIFF	D-M
		1.0				VERY STIFF	
		1.5	WEATHERED SHALE: grey/brown			EXTREMELY LOW STRENGTH	D
			AUGER REFUSAL AT 1.7 M ON WEATHERED SHALE				
		2.0					
		2.5					
	D - disturbe	d sample	U - undisturbed tube sample B - bulk sam	nple	Contracto	r: STS	<u> </u>
		f water table or	free water N - Standard	d Penetration Test (SPT)	Equipmen Hole Diam	t: Mini Christie eter (mm): 100	
NOTES:			See explanation sheets for meaning of all descriptive terms and sy		Angle from Drill Bit: S	vertical (°): 0 piral	

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpor		Project / STS No. 31527/5761D-G		BOREHOLE NO.:	BH 3
		on Street, Dund wing No. 21/366		Date: November 29, 2021 Logged: TS Checked By: IW		Sheet 1 of 1	
W AT TA EB RL E	S A M P L E S	DEPTH (m)	DESCRIPTION OF	DRILLED PRODUCT ity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and	M O I S T U R E
			TOPSOIL: SILTY CLAY: brown, low plasticity		CL	. STIFF	М
		0.5	SILTY CLAY: red brown and mottled orange brown,	medium plasticity, trace of gravel	CL	. STIFF	D-M
	U50						
		1.0	WEATHERED SHALE: dark grey/brown AUGER REFUSAL AT 1.3 M ON WEATHERED SHALE			EXTREMELY LOW STRENGTH	D
		2.0					
		2.5					
	D - disturbe		U - undisturbed tube sample	B - bulk sample		tor: STS	
	WT - level o S - jar sampl	f water table or le	tree water	N - Standard Penetration Test (SPT)		ent: Mini Christie ameter (mm): 100	
NO===	J - jai saiilpi		See explanation sheets for meaning of all description	ve terms and symbols		om Vertical (°): 0	
NOTES:			222 SAPIGNORON SACCES FOR INCOMING OF AN OCSCIPPIN		Drill Bit:		

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpo			BOREHOLE NO.:	BH 4
1		ving No. 21/36			Sheet 1 of 1	
W ATTA EB RL	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B C	RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	S3 @ 0.4 m	0.5	FILL: SILTY CLAY: brown, some red brown and grey, low to medium plasticity, trace of gravel	C	L FIRM TO STIFF	M
		1.0	SILTY CLAY: red brown and mottled orange brown, medium plasticity, trace of gravel	C	L STIFF VERY STIFF	D-M
		1.5	WEATHERED SHALE: grey/brown		EXTREMELY LOW STRENGTH	D
	D. dietusk	2.5	AUGER REFUSAL AT 1.9 M ON WEATHERED SHALE	Contro	etar: CTS	
NOTES:	D - disturbed WT - level of S - jar sampl	f water table o	U - undisturbed tube sample Free water N - Standard Penetration Test (SPT) See explanation sheets for meaning of all descriptive terms and symbols	Equipm Hole Di Angle fr	ector: STS nent: Mini Christie nameter (mm): 100 rom Vertical (°): 0	

GEOTECHNICAL LOG - NON CORE BOREHOLE

	: NSW Land & Housing Corporation :t: 18-28 Simpson Street, Dundas Valley			BOREHOLE NO.: BH 5			
1		on Street, Dund ving No. 21/360			Sheet 1 of 1		
W ATTA EB RL E	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S N E C	RELATIVE DENSITY Sample (sands and gravels)	M O I S T U R E	
			TOPSOIL: SILTY CLAY: brown, low plasticity	C		M	
	S4 @ 0.4 m	0.5	SILTY CLAY: red brown and mottled orange brown, medium plasticity, trace of gravel	С	L STIFF	D-M	
	U50	1.0			VERY STIFF		
		1.5	WEATHERED SHALE: grey/brown		EXTREMELY LOW STRENGTH	D	
		2.0	AUGER REFUSAL AT 1.8 M ON WEATHERED SHALE				
		2.5					
NOTES:	D - disturbed WT - level of S - jar sampl	f water table o	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT) See explanation sheets for meaning of all descriptive terms and symbols	Equipm Hole Di	ctor: STS nent: Mini Christie iameter (mm): 100 rom Vertical (°): 0		
				Drill Bit	t: Spiral		

GEOTECHNICAL LOG - NON CORE BOREHOLE

Client:		Housing Corpo			BOREHOLE NO.:	BH 6
1		ving No. 21/366			Sheet 1 of 1	
W ATTA EB RL E	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	RELATIVE DENSITY (sands and gravels)	M O I S T U R E
	\$5		TOPSOIL: SILTY CLAY: brown, some grey, low to medium plasticity, trace of gravel	CL	FIRM TO STIFF	M
	@ 0.4 m	0.5	SILTY CLAY: red brown and mottled orange brown, medium plasticity, trace of gravel	CL	. STIFF	D-M
		1.0			VERY STIFF	
		1.5	WEATHERED SHALE: grey/brown		EXTREMELY LOW STRENGTH	D
		2.0	AUGER REFUSAL AT 1.9 M ON WEATHERED SHALE			
		2.5				
NOTES:	D - disturbed WT - level of S - jar sampl	f water table or	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT) See explanation sheets for meaning of all descriptive terms and symbols	Equipme Hole Dia	tor: STS ent: Mini Christie ameter (mm): 100 om Vertical (°): 0	
				Drill Bit:		

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpo			BOREHOLE NO.:	BH 7
1		on Street, Dunc ving No. 21/36			Sheet 1 of 1	
W ATTA EB RL	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L		M O I S T U R E
			TOPSOIL: SILTY CLAY: brown, low plasticity	CL	FIRM TO STIFF	M
		0.5	SILTY CLAY: red brown and mottled orange brown, medium plasticity, trace of gravel	CL	FIRM TO STIFF BECOMING STIFF	D-M
	U50	1.0			VERY STIFF	
		1.5	WEATHERED SHALE: grey/brown AUGER REFUSAL AT 1.6 M ON WEATHERED SHALE		EXTREMELY LOW STRENGTH	D
		2.0				
		2.5				
	D - disturbed WT - level of S - jar sampl	f water table o	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT) See explanation sheets for meaning of all descriptive terms and symbols	Hole Dia	ent: Mini Christie ameter (mm): 100	
NOTES:			See explanation sheets for meaning of an descriptive terms and symbols	Drill Bit:	om Vertical (°): 0 Spiral	

GEOTECHNICAL LOG - NON CORE BOREHOLE

		Housing Corpor			ВС	OREHOLE NO.:	BH 8	
II -		on Street, Dund wing No. 21/366		\vdash	Sheet 1 of 1			
W AT TA EB RL	S A M P L E	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)		S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E	
			TOPSOIL: SILTY CLAY: brown, low plasticity		CL	FIRM TO STIFF	М	
	S6 @ 0.4 m	0.5	SILTY CLAY: red brown and mottled orange brown/grey, medium plasticity, trace of gravel		CL	FIRM TO STIFF BECOMING STIFF	D-M	
					•	VERY STIFF		
		1.0						
		1.5	SILTY CLAY: light grey, mottled reed brown, medium plasticity	1	CL		D-M	
			WEATHERED SHALE: grey/brown			EXTREMELY LOW STRENGTH	D	
		2.0	AUGER REFUSAL AT 1.9 M ON WEATHERED SHALE					
		2.5						
		_						
	D - disturbe WT - level o S - jar samp	f water table or	U - undisturbed tube sample B - bulk sample free water N - Standard Penetration Test (SPT)		ment:	: STS : Mini Christie eter (mm): 100		
NOTES:			See explanation sheets for meaning of all descriptive terms and symbols	Angle Drill B		Vertical (°): 0 piral		



14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Dynamic Cone Penetrometer Test Report

Project: 18-28 SIMPSON STREET, DUNDAS VALLEY Project No.: 31527/5761D

Client: NSW LAND & HOUSING CORPORATION

Report No.: 21/3668

Address: Level G, 12 Darcy Street, Parramatta

Report Date: 7/12/2021

Test Method: AS 1289.6.3.2

Page: 1 of 2

	,					
Site No.	P1	P2	Р3	P4	P5	P6
Location	Refer to Drawing No. 21/3669					
Date Tested	29/11/2021	29/11/2021	29/11/2021	29/11/2021	29/11/2021	29/11/2021
Starting Level	Surface Level	Surface Level	Surface Level	Surface Level	Surface Level	Surface Level
Depth (m)		Pe	netration Resistar	nce (blows / 150m	m)	
0.00 - 0.15	3	5	5	2	3	4
0.15 - 0.30	4	4	6	3	4	5
0.30 - 0.45	4	5	6	4	7	6
0.45 - 0.60	8	5	7	4	6	4
0.60 - 0.75	7	6	6	5	6	5
0.75 - 0.90	7	8	22/R	5	5	6
0.90 - 1.05	9	10		7	8	6
1.05 - 1.20	13	22/R		10	7	7
1.20 - 1.35	22/R			10	22/R	9
1.35 - 1.50				22/R		22/R
1.50 - 1.65						
1.65 - 1.80						
1.80 - 1.95						
1.95 - 2.10						
2.10 - 2.25						
2.25 - 2.40						
2.40 - 2.55						
2.55 - 2.70						
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: * Pre drilled prior to testing

TS

Technician:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Form: RPS26 Date of Issue: 31/05/21 Revision: 2



14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Dynamic Cone Penetrometer Test Report

Project: 18-28 SIMPSON STREET, DUNDAS VALLEY Project No.: 31527/5761D

Client: NSW LAND & HOUSING CORPORATION

Report No.: 21/3668

Address: Level G, 12 Darcy Street, Parramatta

Report Date: 7/12/2021

Test Method: AS 1289.6.3.2 Page: 2 of 2

Site No.	P7	P8				
Location	Refer to Drawing No. 21/3669	Refer to Drawing No. 21/3669				
Date Tested	29/11/2021	29/11/2021				
Starting Level	Surface Level	Surface Level				
Depth (m)		Pe	netration Resistar	nce (blows / 150m	m)	
0.00 - 0.15	5	6				
0.15 - 0.30	4	4				
0.30 - 0.45	3	3				
0.45 - 0.60	5	6				
0.60 - 0.75	5	7				
0.75 - 0.90	6	7				
0.90 - 1.05	13	8				
1.05 - 1.20	22/R	13				
1.20 - 1.35		17				
1.35 - 1.50		22/R				
1.50 - 1.65						
1.65 - 1.80						
1.80 - 1.95						
1.95 - 2.10						
2.10 - 2.25						
2.25 - 2.40						
2.40 - 2.55						
2.55 - 2.70						
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: * Pre drilled prior to testing

TS

Technician:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Form: RPS26 Date of Issue: 31/05/21 Revision: 2

E1. CLASSIFICATION OF SOILS

E1.1 Soil Classification and the Unified System

An assessment of the site conditions usually includes an appraisal of the data available by combining values of engineering properties obtained by the site investigation with descriptions, from visual observation of the materials present on site.

The system used by STS Geotechnics Pty Ltd (STS) in the identification of soil is the Unified Soil Classification system (USC) which was developed by the US Army Corps of Engineers during World War II and has since gained international acceptance and has been adopted in its metricated form by the Standards Association of Australia.

The Australian Site Investigation Code (AS1726-1981, Appendix D) recommends that the description of a soil includes the USC group symbols which are an integral component of the system.

The soil description should contain the following information in order:

Soil composition

- SOIL NAME and USC classification symbol (IN BLOCK LETTERS)
- plasticity or particle characteristics
- colour
- secondary and minor constituents (name estimated proportion, plasticity or particle characteristics, colour

Soil condition

- moisture condition
- consistency or density index

Soil structure

• structure (zoning, defects, cementing)

Soil origin

interpretation based on observation eg FILL, TOPSOIL, RESIDUAL, ALLUVIUM.

E1.2 Soil Composition

(a) Soil Name and Classification Symbol

The USC system is summarised in Figure E1.2.1. The primary division separates soil types on the basis of particle size into:

- Coarse grained soils more than 50% of the material less than 60 mm is larger than 0.06 mm (60 μm).
- Fine grained soils more than 50% of the material less than 60 mm is smaller than 0.06 mm (60 μ m).

Initial classification is by particle size as shown in Table E1.2.1. Further classification of fine grained soils is based on plasticity.

TABLE E1.2.1 - CLASSIFICATION BY PARTICLE SIZE

NAME	SUB-DIVISION	SIZE
Clay (1)		< 2 μm
Silt (2)		2 μm to 60 μm
Sand	Fine Medium Coarse	60 μm to 200 μm 200 μm to 600 μm 600 μm to 2 mm
Gravel (3)	Fine Medium Coarse	2 mm to 6 mm 6 mm to 20 mm 20 mm to 60 mm
Cobbles (3)		60 mm to 200 mm
Boulders (3)		> 200 mm

Where a soil contains an appropriate amount of secondary material, the name includes each of the secondary components (greater than 12%) in increasing order of significance, eg sandy silty clay.

Minor components of a soil are included in the description by means of the terms "some" and "trace" as defined in Table E1.2.2.

TABLE E1.2.2 - MINOR SOIL COMPONENTS

TERM	DESCRIPTION	APPROXIMATE PROPORTION (%)
Trace	presence just detectable, little or no influence on soil properties	0-5
Some	presence easily detectable, little influence on soil properties	5-12

The USC group symbols should be included with each soil description as shown in Table E1.2.3

TABLE E1.2.3 - SOIL GROUP SYMBOLS

SOIL TYPE	PREFIX
Gravel	G
Sand	S
Silt	M
Clay	С
Organic	О
Peat	Pt

The group symbols are combined with qualifiers which indicate grading, plasticity or secondary components as shown on Table E1.2.4

TABLE E1.2.4 - SOIL GROUP QUALIFIERS

SUBGROUP	SUFFIX
Well graded	W
Poorly Graded	P
Silty	M
Clayey	C
Liquid Limit <50% - low to medium plasticity	L
Liquid Limit >50% - medium to high plasticity	Н

(b) Grading

"Well graded" Good representation of all

particle sizes from the largest

to the smallest.

"Poorly graded" One or more intermediate

sizes poorly represented

"Gap graded" One or more intermediate

sizes absent

"Uniformly graded" Essentially single size

material.

(c) Particle shape and texture

The shape and surface texture of the coarse grained particles should be described.

Angularity may be expressed as "rounded", "subrounded", "sub-angular" or "angular".

Particle **form** can be "equidimensional", "flat" or elongate".

Surface texture can be "glassy", "smooth", "rough", pitted" or striated".

(d) Colour

The colour of the soil should be described in the moist condition using simple terms such as:

> Black White Grey Red Brown Orange Yellow Green Blue

These may be modified as necessary by "light" or "dark". Borderline colours may be described as a combination of two colours, eg red-brown.

For soils that contain more than one colour terms such as:

• Speckled Very small (<10 mm dia) patches

• Mottled Irregular

• Blotched Large irregular (>75 mm dia)

• Streaked Randomly oriented streaks

(e) Minor Components

Secondary and minor components should be individually described in a similar manner to the dominant component.

E1.3 Soil Condition

(a) Moisture

Soil moisture condition is described as "dry", "moist" or "wet".

The moisture categories are defined as:

Dry (D) - Little or no moisture evident. Soils are running. Moist (M) - Darkened in colour with cool feel. Granular soil particles tend to adhere. No free water evident upon remoulding of cohesive soils.

In addition the moisture content of cohesive soils can be estimated in relation to their liquid or plastic limit.

(b) Consistency

Estimates of the consistency of a clay or silt soil may be made from manual examination, hand penetrometer test, SPT results or from laboratory tests to determine undrained shear or unconfined compressive strengths. The classification of consistency is defined in Table E1.3.1.

TABLE E1.3.1 - CONSISTENCY OF FINE-GRAINED SOILS

TERM	UNCONFINED STRENGTH (kPa)	FIELD IDENTIFICATION
Very Soft	<25	Easily penetrated by fist. Sample exudes between fingers when squeezed in the fist.
Soft	25 - 50	Easily moulded in fingers. Easily penetrated 50 mm by thumb.
Firm	50 - 100	Can be moulded by strong pressure in the fingers. Penetrated only with great effort.
Stiff	100 - 200	Cannot be moulded in fingers. Indented by thumb but penetrated only with great effort.
Very Stiff	200 - 400	Very tough. Difficult to cut with knife. Readily indented with thumb nail.
Hard	>400	Brittle, can just be scratched with thumb nail. Tends to break into fragments.

Unconfined compressive strength as derived by a hand penetrometer can be taken as approximately double the undrained shear strength $(q_u = 2 \ c_u)$.

(c) Density Index

The insitu density index of granular soils can be assessed from the results of SPT or cone penetrometer tests. Density index should not be estimated visually.

TABLE E1.3.2 - DENSITY OF GRANULAR SOILS

TERM	SPT N	STATIC	DENSITY
	VALUE	CONE	INDEX
		VALUE	(%)
		q _c (MPa)	
Very Loose	0 - 3	0 - 2	0 - 15
Loose	3 - 8	2 - 5	15 - 35
Medium Dense	8 - 25	5 - 15	35 - 65
Dense	25 - 42	15 - 20	65 - 85
Very Dense	>42	>20	>85

E1.4 Soil Structure

(a) Zoning

A sample may consist of several zones differing in colour, grain size or other properties. Terms to classify these

Layer - continuous across exposure or sample

Lens - discontinuous with lenticular shape

Pocket - irregular inclusion

Each zone should be described, their distinguishing features, and the nature of the interzone boundaries.

(b) Defects

Defects which are present in the sample can include:

- fissures
- roots (containing organic matter)
- tubes (hollow)
- · casts (infilled)

Defects should be described giving details of dimensions and frequency. Fissure orientation, planarity, surface condition and infilling should be noted. If there is a tendency to break into blocks, block dimensions should be recorded

E1.5 Soil Origin

Information which may be interpretative but which may contribute to the usefulness of the material description should be included. The most common interpreted feature is the origin of the soil. The assessment of the probable origin is based on the soil material description, soil structure and its relationship to other soil and rock materials.

Common terms used are:

"Residual Soil" - Material which appears to have been derived by weathering from the underlying rock. There is no evidence of transport.

"Colluvium" - Material which appears to have been transported from its original location. The method of movement is usually the combination of gravity and erosion

"Landslide Debris" - An extreme form of colluvium where the soil has been transported by mass movement. The material is obviously distributed and contains distinct defects related to the slope failure.

"Alluvium" - Material which has been transported essentially by water. usually associated with former stream activity.

"Fill" - Material which has been transported and placed by man. This can range from natural soils which have been placed in a controlled manner in engineering construction to dumped waste material. A description of the constituents should include an assessment of the method of placement.

E1.6 Fine Grained Soils

The physical properties of fine grained soils are dominated by silts and clays.

The definition of clay and silt soils is governed by their Atterberg Limits. Clay soils are characterised by the properties of cohesion and plasticity with cohesion defines as the ability to deform without rupture. Silts exhibit cohesion but have low plasticity or are non-plastic.

The field characteristics of clay soils include:

- dry lumps have appreciable dry strength and cannot be powdered
- volume changes occur with moisture content variation
- feels smooth when moist with a greasy appearance when cut.

The field characteristics of silt soils include:

- dry lumps have negligible dry strength and can be powdered easily
- dilatancy an increase in volume due to shearing is indicted by the presence of a shiny film of water after a hand sample is shaken. The water disappears upon remoulding. Very fine grained sands may also exhibit dilatancy.
- low plasticity index
- feels gritty to the teeth

E1.7 Organic Soils

Organic soils are distinguished from other soils by their appreciable content of vegetable matter, usually derived from plant remains.

The soil usually has a distinctive smell and low bulk density.

The USC system uses the symbol Pt for partly decomposed organic material. The O symbol is combined with suffixes "O" or "H" depending on plasticity.

Where roots or root fibres are present their frequency and the depth to which they are encountered should be recorded. The presence of roots or root fibres does not necessarily mean the material is an "organic material" by classification.

Coal and lignite should be described as such and not simply as organic matter.



APPENDIX B - LABORATORY TEST RESULTS



14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Shrink Swell Index Report

Project: 18 - 28 SIMPSON STREET, DUNDAS VALLEY

Client: NSW LAND & HOUSING CORPORATION

Address: Level 2, 31-39 Macquarie Street, Parramatta 2150

Test Method: AS1289.7.1.1

Project No.: 31527

Report No.: 21/3632

Report Date: 6/12/2021

Page: 1 OF 1

Sampling Procedure: AS 1289.1.3.1 Clause 3.1.3.2 - Thin Walled Sampler

STS / Sample No.		5761D-L/1	5761D-L/2	5761D-L/3	5761D-L/4	
Sample Location		Borehole 1 Refer to Drawing	Borehole 3 Refer to Drawing	Borehole 5 Refer to Drawing	Borehole 7 Refer to Drawing	
Material Description		Gravelly Sandy Clay, red brown/red	Gravelly Silty Sandy Clay, orange brown	Silty Clay, red brown, trace of gravel/sand	Gravelly Silty Clay, red brown/yellow	
Depth (m)		0.7 - 0.9	0.7 - 0.85	0.7 - 0.9	0.7 - 0.9	
Sample Date		29/11/2021	29/11/2021	29/11/2021	29/11/2021	
	Moisture Content (%)	23.3	12.9	25.9	23.8	
Shrink	Soil Crumbling	Nil	Nil	Nil	Nil	
Shr	Extent of Cracking	Fine Cracks	Open Cracks	Nil	Open Cracks	
	Strain (%)	3.1	1.0	4.5	2.8	
	Moisture Content Initial (%)	23.8	20.1	27.0	30.7	
Swell	Moisture Content Final (%)	25.6	24.0	29.5	30.9	
	Strain (%)	0.2	0.7	1.3	0.2	
Inert Inclusions (%)		<30	<30	<10	<40	
Shrink Swell Index (%)		1.8	0.8	2.9	1.6	

Remarks:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Technician: DH

Form: RPS41 Date of Issue: 31/05/21



CERTIFICATE OF ANALYSIS

Work Order : ES2143710

: STS Geotechnics Contact

: ENQUIRES STS

Address : Unit 14/1 Cowpasture Place

Wetherill Park 2164

Telephone

Client

Project : 30055/30060/31527/31555

Order number : E-2021-0419

C-O-C number Sampler Site Quote number : EN/222

No. of samples received : 16 No. of samples analysed : 16 Page : 1 of 6

Laboratory : Environmental Division Sydney

Contact : Customer Services ES

Address : 277-289 Woodpark Road Smithfield NSW Australia 2164

Telephone : +61-2-8784 8555 **Date Samples Received** : 01-Dec-2021 12:50

Date Analysis Commenced : 02-Dec-2021

Issue Date · 06-Dec-2021 16:25



This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with **Quality Review and Sample Receipt Notification.**

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories Position Accreditation Category

Ankit Joshi Inorganic Chemist Sydney Inorganics, Smithfield, NSW Sydney Inorganics, Smithfield, NSW Wisam Marassa Inorganics Coordinator

Page : 2 of 6
Work Order : ES2143710

Client : STS Geotechnics

Project : 30055/30060/31527/31555



General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

- ^ = This result is computed from individual analyte detections at or above the level of reporting
- ø = ALS is not NATA accredited for these tests.
- ~ = Indicates an estimated value.

Page : 3 of 6
Work Order : ES2143710

Client : STS Geotechnics
Project : 30055/30060/31527/31555



Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	30055/8023	30055/8024	30055/8044	30055/8047	30060/1558
		Sampli	ng date / time	30-Nov-2021 00:00				
Compound	CAS Number	LOR	Unit	ES2143710-001	ES2143710-002	ES2143710-003	ES2143710-004	ES2143710-005
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	7.6	7.8	7.3	8.3	8.0
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	115	281	257	238	176
EA055: Moisture Content (Dried @ 105	i-110°C)							
Moisture Content		0.1	%	15.8	7.3	12.0	12.9	12.4
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	20	220	160	120	80

Page : 4 of 6
Work Order : ES2143710

Client : STS Geotechnics
Project : 30055/30060/31527/31555



Sub-Matrix: SOIL (Matrix: SOIL)	Sample ID				30060/1561	30060/1562	30060/1563	31527/S1
		Sampli	ng date / time	30-Nov-2021 00:00				
Compound	CAS Number	LOR	Unit	ES2143710-006	ES2143710-007	ES2143710-008	ES2143710-009	ES2143710-010
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	8.5	8.2	8.7	7.2	5.9
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	532	207	287	41	30
EA055: Moisture Content (Dried @ 105-11	10°C)							
Moisture Content		0.1	%	10.2	12.0	10.2	23.0	21.0
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	250	60	80	10	<10
ED045G: Chloride by Discrete Analyser								
Chloride	16887-00-6	10	mg/kg					120

Page : 5 of 6
Work Order : ES2143710

Client : STS Geotechnics
Project : 30055/30060/31527/31555



Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	31527/S2	31527/S3	31527/S4	31527/S5	31527/S6
		Sampli	ng date / time	30-Nov-2021 00:00				
Compound	CAS Number	LOR	Unit	ES2143710-011	ES2143710-012	ES2143710-013	ES2143710-014	ES2143710-015
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	5.4	5.9	5.1	6.3	5.6
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	14	19	34	19	36
EA055: Moisture Content (Dried @ 105-1	10°C)							
Moisture Content		0.1	%	20.3	21.0	22.4	21.6	25.5
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	<10	10	30	10	40
ED045G: Chloride by Discrete Analyser								
Chloride	16887-00-6	10	mg/kg	40	60	<10	90	20

Page : 6 of 6
Work Order : ES2143710

Client : STS Geotechnics
Project : 30055/30060/31527/31555



Sub-Matrix: SOIL (Matrix: SOIL)	Sample ID			31555/S1	 	
		Sampli	ng date / time	30-Nov-2021 00:00	 	
Compound	CAS Number	LOR	Unit	ES2143710-016	 	
				Result	 	
EA002: pH 1:5 (Soils)						
pH Value		0.1	pH Unit	6.4	 	
EA010: Conductivity (1:5)						
Electrical Conductivity @ 25°C		1	μS/cm	18	 	
EA055: Moisture Content (Dried @ 105-1	110°C)					
Moisture Content		0.1	%	14.4	 	
ED040S : Soluble Sulfate by ICPAES						
Sulfate as SO4 2-	14808-79-8	10	mg/kg	<10	 	
ED045G: Chloride by Discrete Analyser						
Chloride	16887-00-6	10	mg/kg	20	 	